

Design Process for the Advanced Photon Source Fast Orbit Feedback System Upgrade

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Advanced Photon Source
**Workshop on Next-Generation
Fast Orbit Feedback Systems for
Storage Rings**
May 9, 2013

Design Philosophy

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Design Philosophy

- What is and was necessarily influences what shall be.
- What shall be supersedes what can possibly be.
- What can possibly be should be within grasp of what shall in fact be.
- What now is provides enormous leverage towards what shall, or can possibly be.
 - If only we have the conviction to learn from our mistakes past, present, and future.

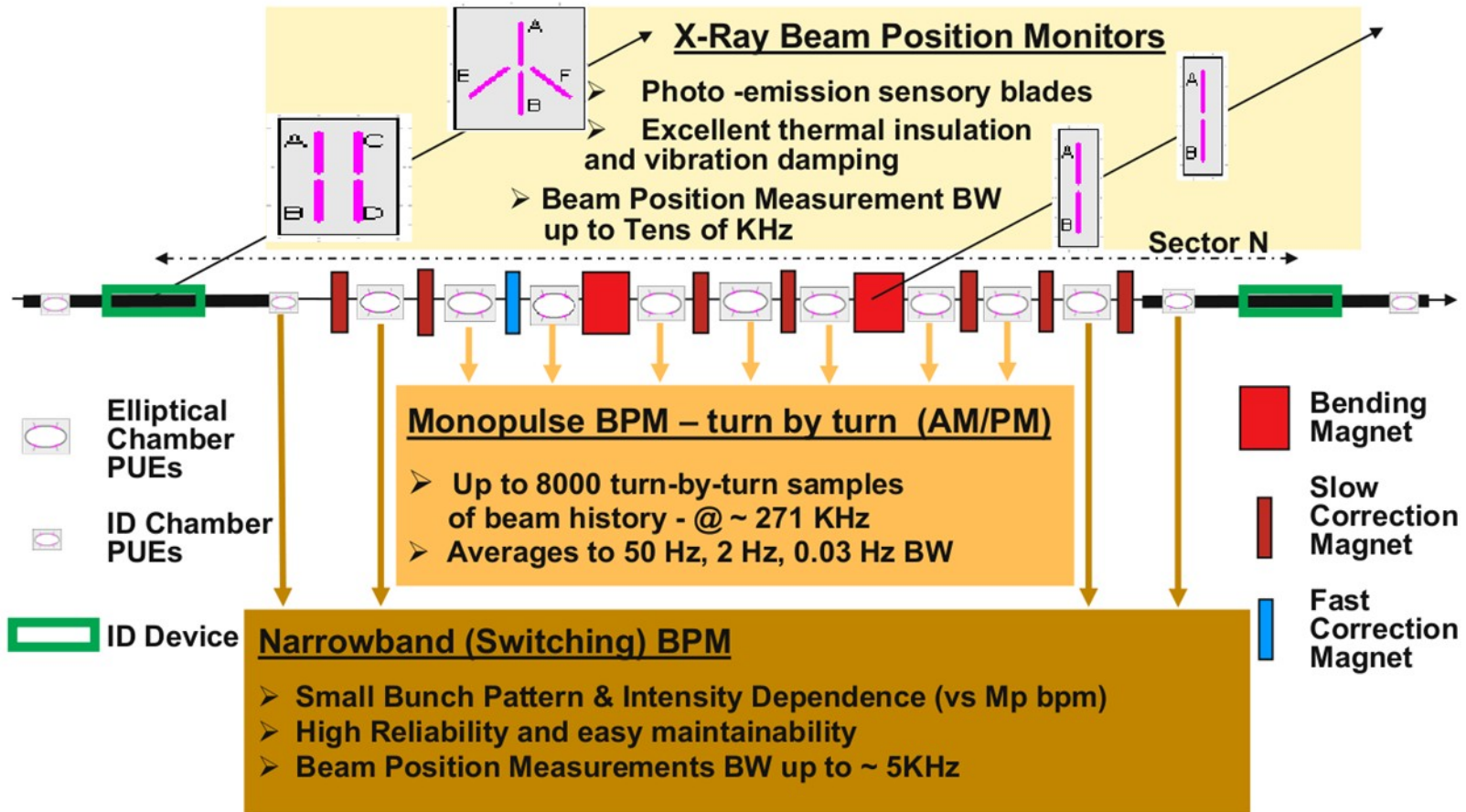


Design Process

- The hardware and interfaces, while challenging, will be straightforward.
- The algorithms to be run on the hardware is perhaps more challenging.
- We have a machine, soon to have a full complement of turn-by-turn bpms.
- We will use the machine we have to simulate the machine we want.
 - Based on measured beam temporal and spatial structure
 - Based on measured steering corrector response
 - Using already-familiar operational orbit correction configuration tools
- An extensive code validation phase will compare simulation with experiment.
- Only then will we start extrapolating.

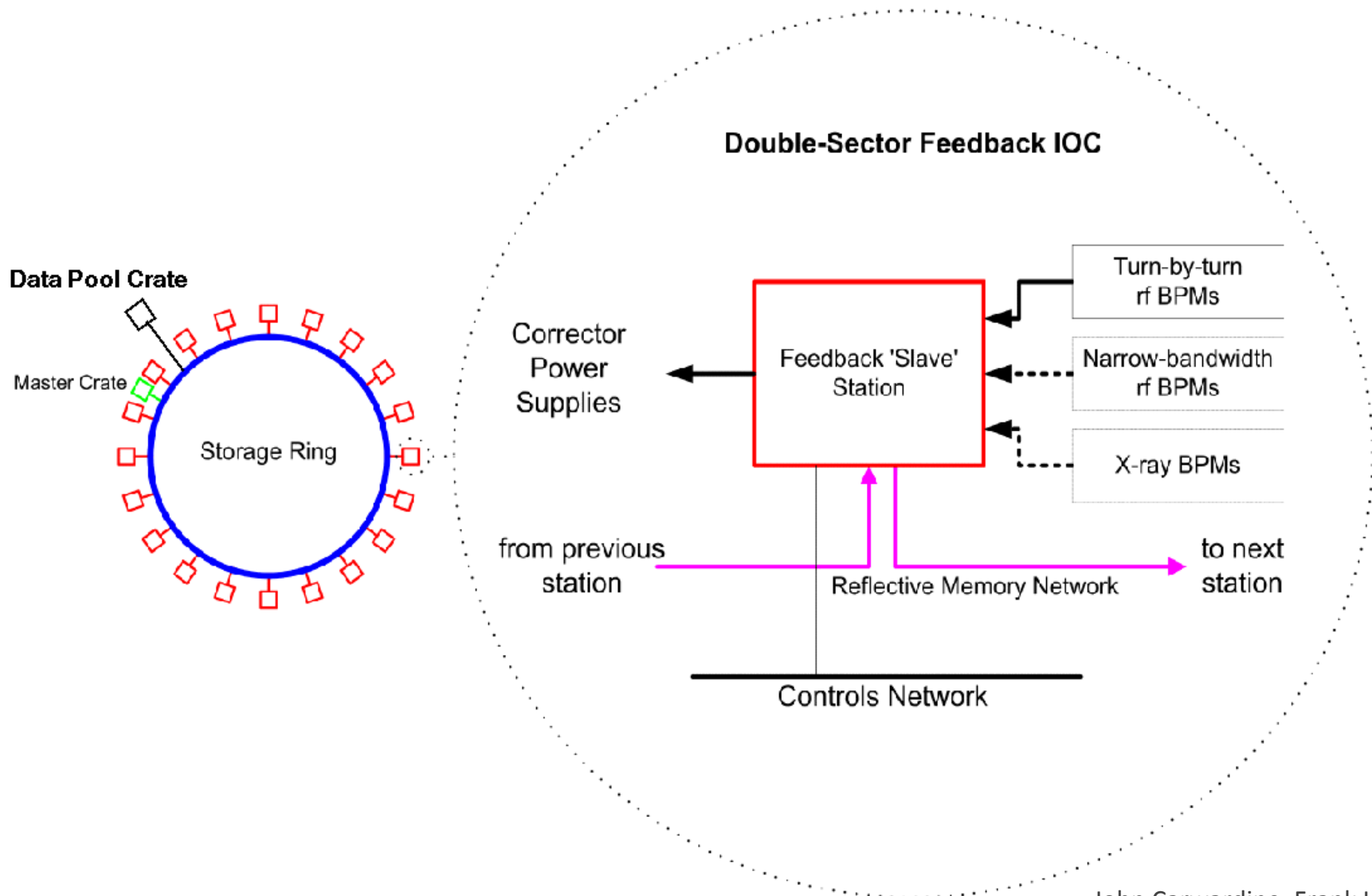


What is and was - APS Beam Position Monitoring



Om Singh c. 2004

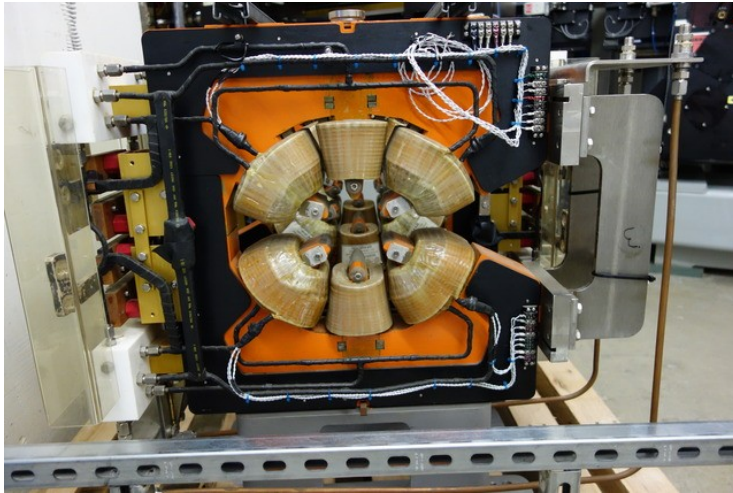
Existing APS Fast Orbit Feedback Architecture



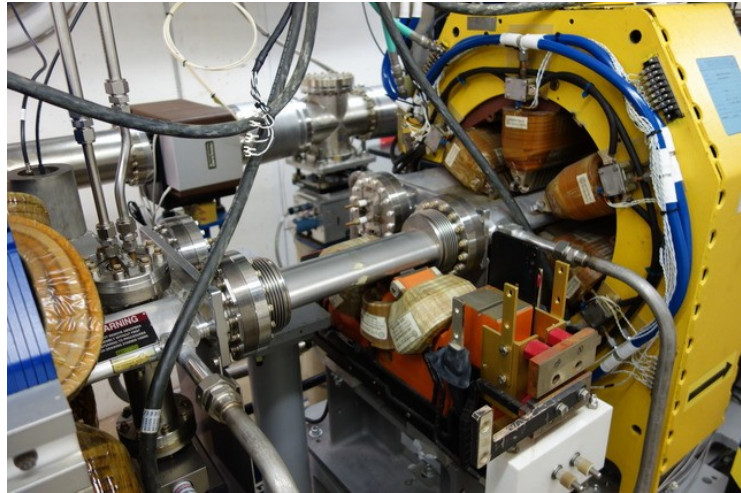
John Carwardine, Frank Lenkszus



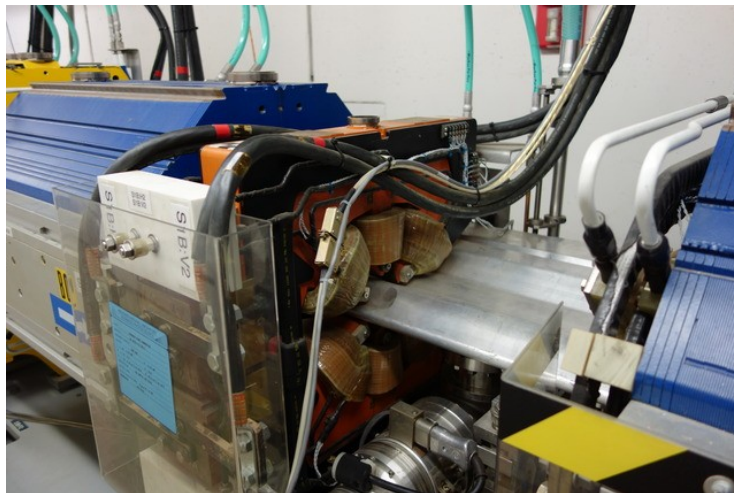
The Hardware



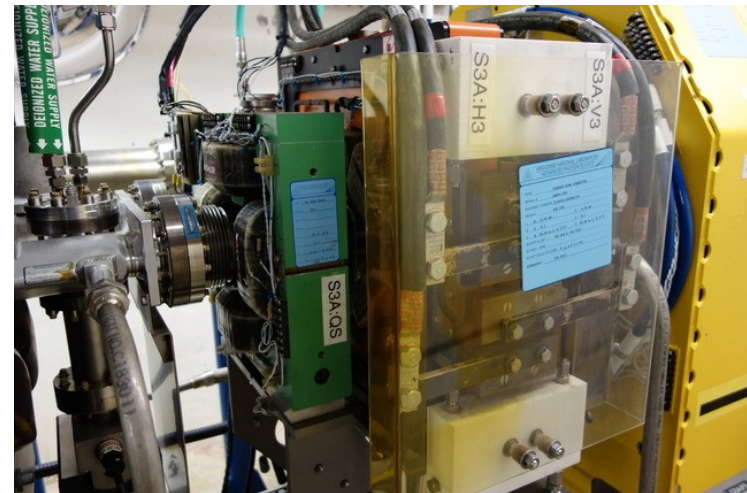
Six-pole combined H/V correctors



Split fast corrector with spool piece
(Note xrbm in background)



Slow corrector with aluminum chamber



Fast corrector with solid-core skew quad



Pickup Electrodes



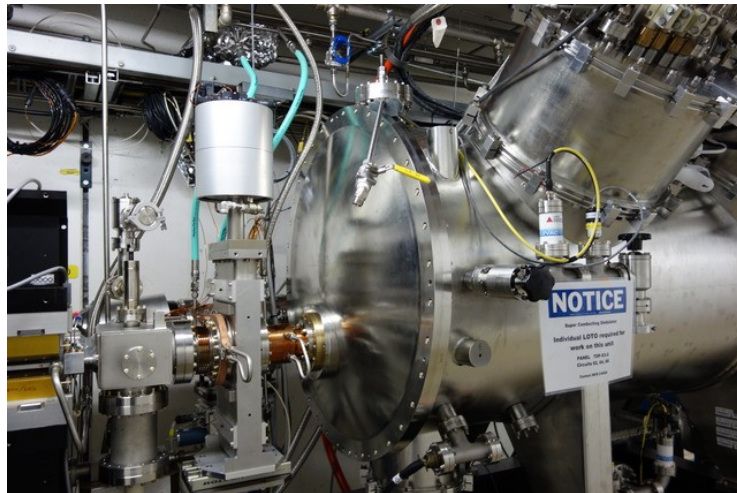
1-cm dia. buttons



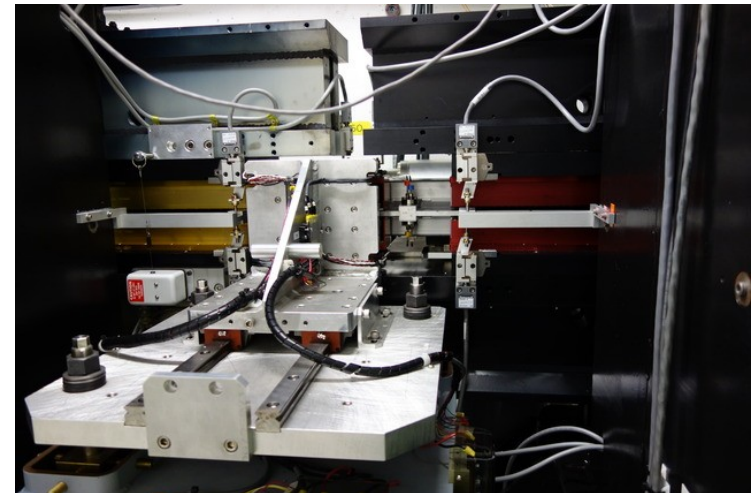
With 352 MHz matching networks



4-mm dia. Buttons @ IDs



Between hybrid undulator and SCU



Between two hybrid undulators

Electronics

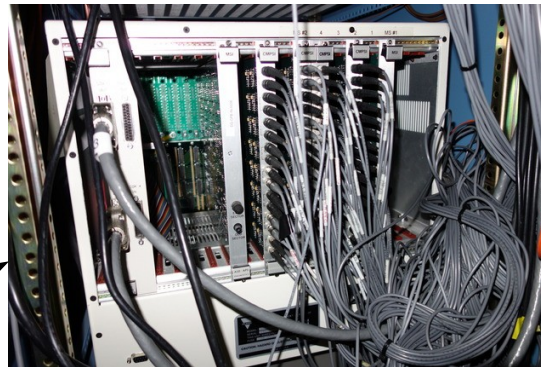


Bergoz

Feedback
Crate
Front
Rear

BSP-100s

Monopulse
Receivers

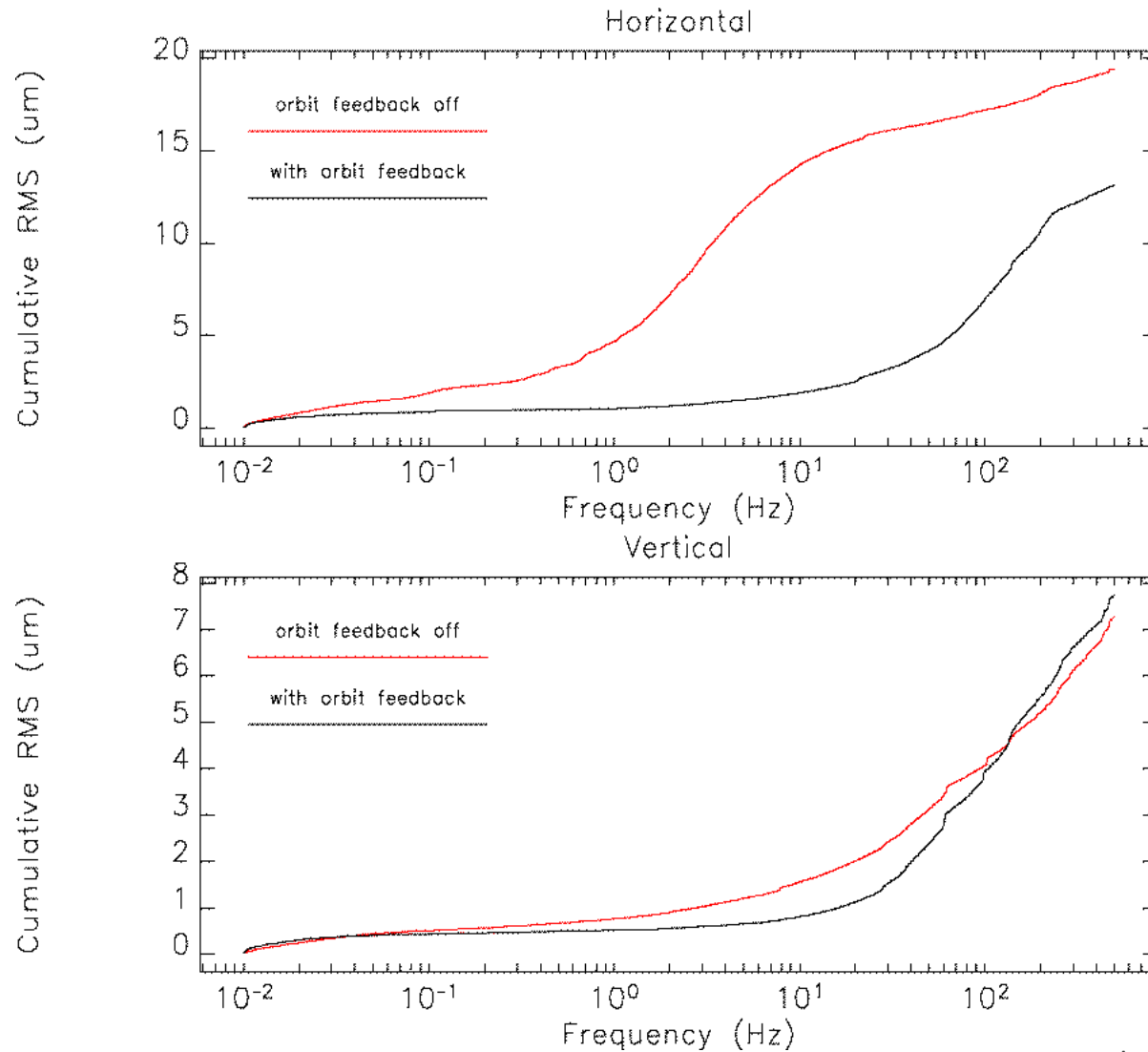


Every corrector gets
two fibers



X-ray BPM Preamps

Existing Feedback Performance

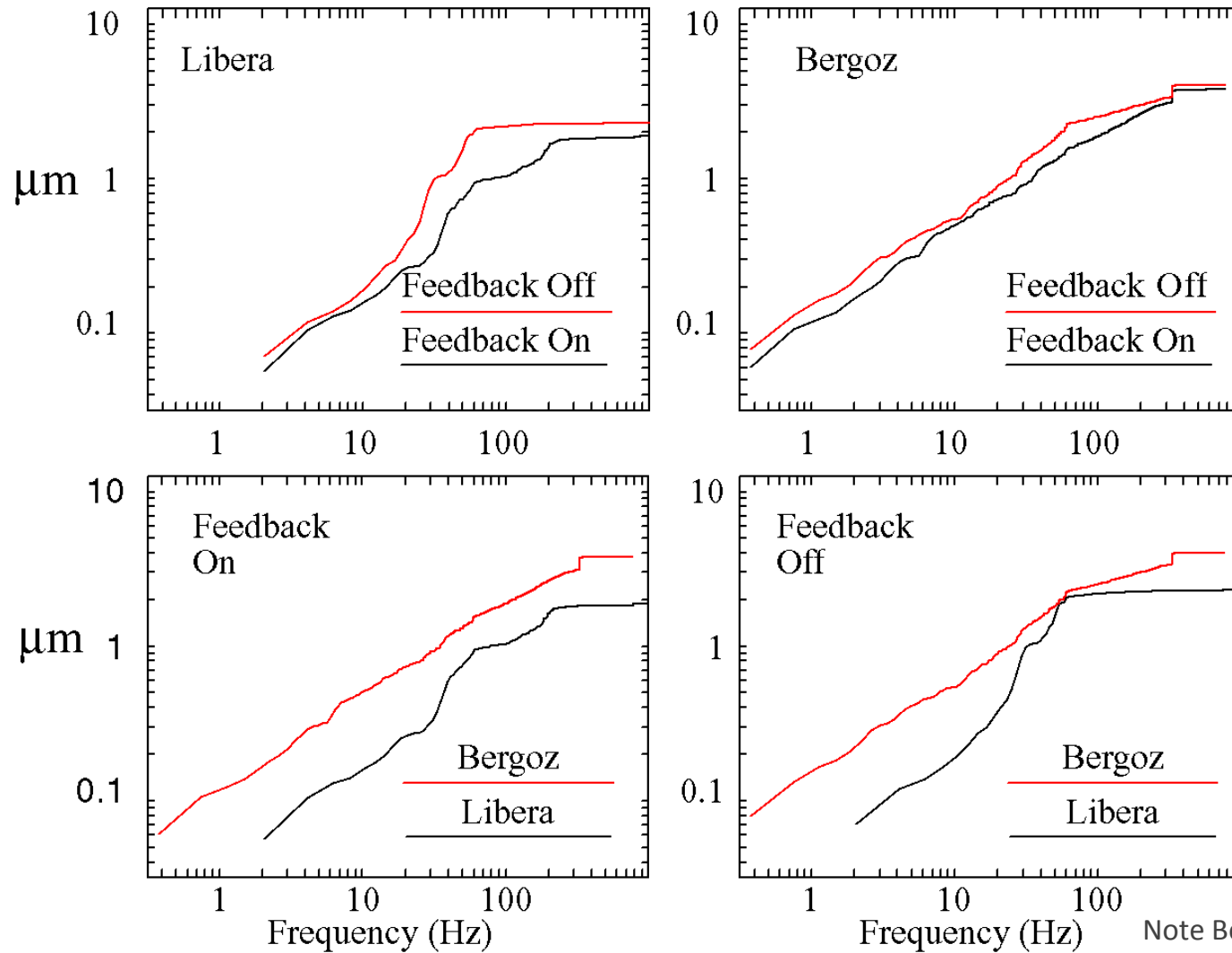


John Carwardine



Noisy BPMs

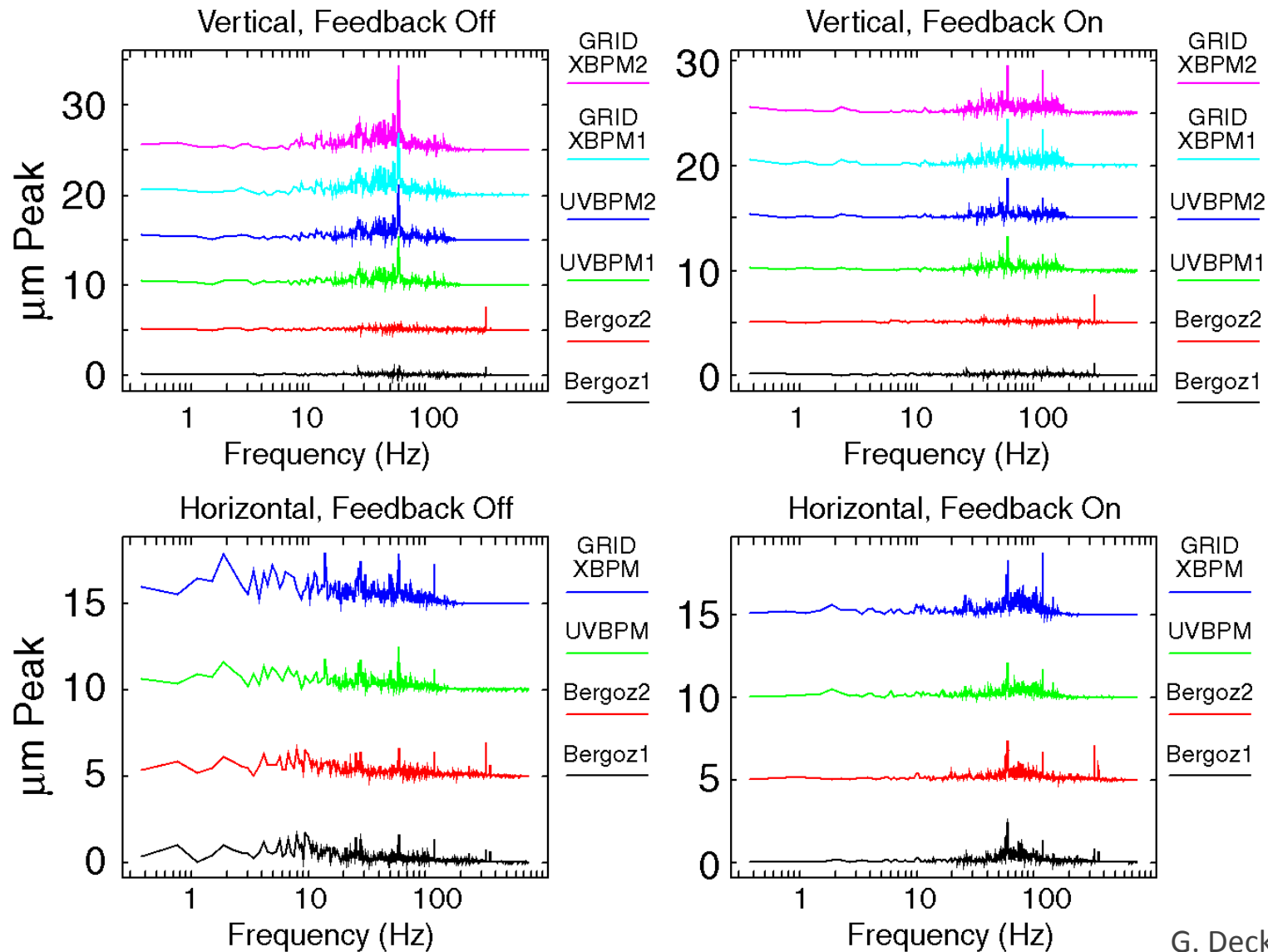
Vertical Comparison, Libera to Bergoz



Note Bergoz w/ 1 cm buttons
Libera w/ 4 mm buttons



Existing Performance Cont'd



G. Decker BIW10



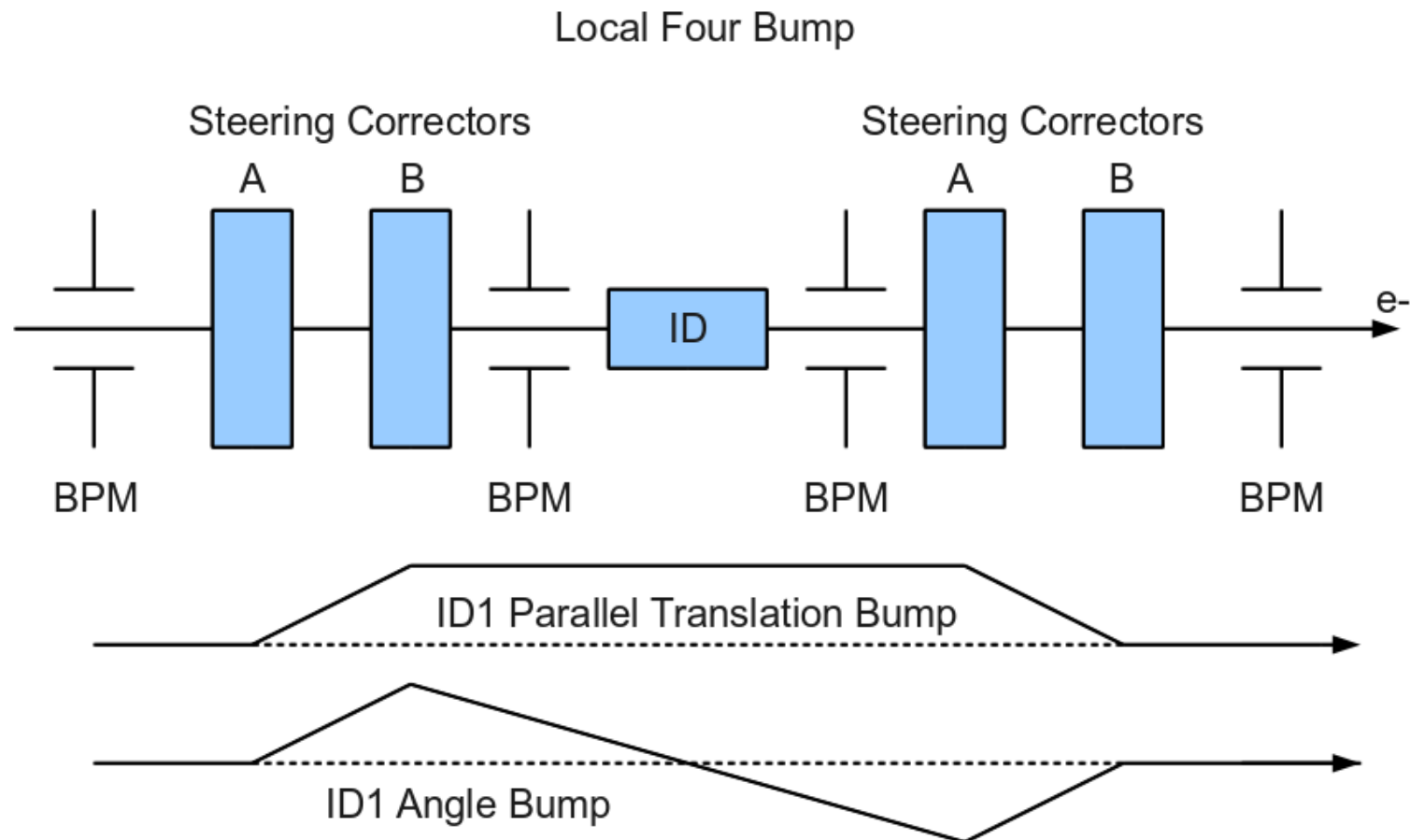
Present and Future Beam Stability

		AC rms motion 0.01-200 Hz		AC rms motion 0.01-1000 Hz		Long-term drift (One Week)	
		$\mu\text{m rms}$	$\mu\text{rad rms}$	$\mu\text{m rms}$	$\mu\text{rad rms}$	$\mu\text{m rms}$	$\mu\text{rad rms}$
Horizontal	Present	5.0	0.85	5.0 - 7.0*	NA	7.0	1.4
	Upgrade	3.0	0.53	6.0	1.14	5.0	1.0
Vertical	Present	1.6	0.80	3.7*	NA	5.0	2.5
	Upgrade	0.42	0.22	0.84	0.44	1.0	0.5

* Measurement up to 767 Hz.

- Based on 5% of transverse beam dimensions up to 200 Hz and 10% up to 1 kHz.

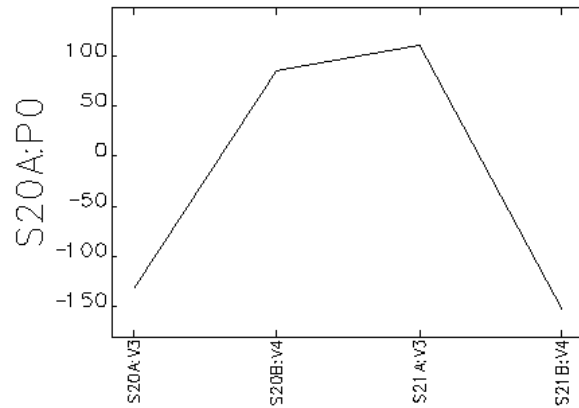
Digression: Spatial Modes 1 - Local Bump



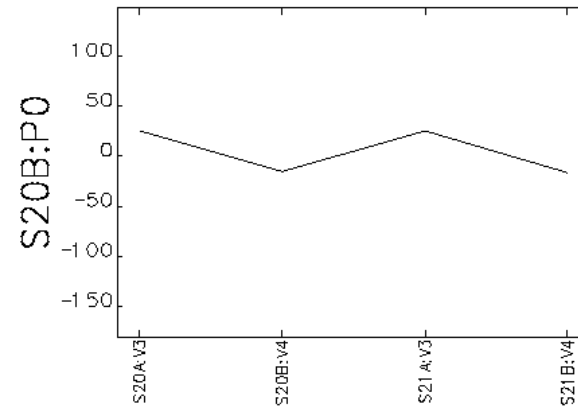
4 by 4 Local Bump Inverse Response Matrix

$$Y_m = R_{mn} C_n \quad R = U S V^T \quad C_n = R_{nm}^{-1} Y_m$$

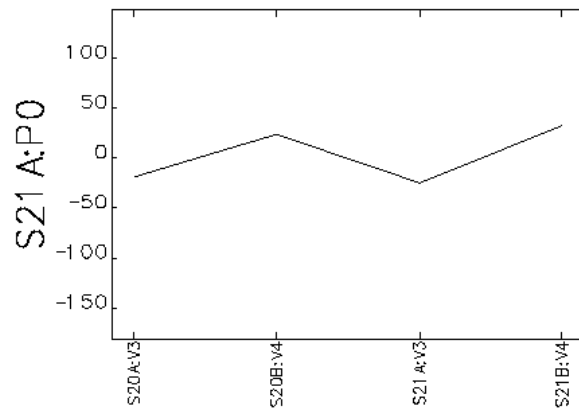
BPMs



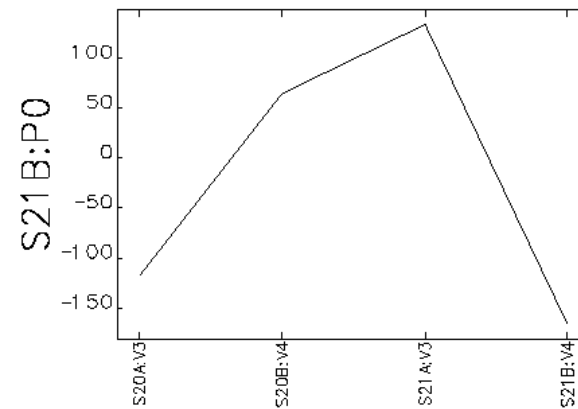
Pseudo-inverse of vertical-plane orbit feed path-length response matrix for beamline RING of lattice optics



Pseudo-inverse of vertical-plane orbit feed path-length response matrix for beamline RING of lattice optics



Pseudo-inverse of vertical-plane orbit feed path-length response matrix for beamline RING of lattice optics



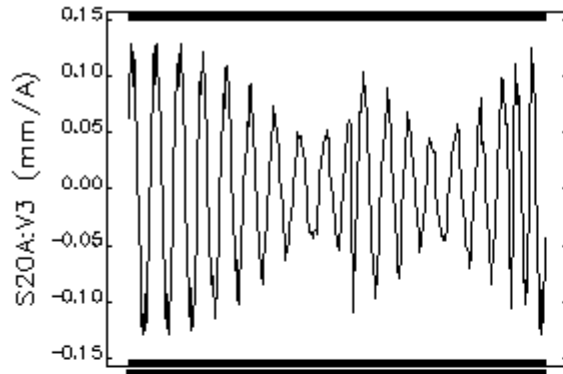
Pseudo-inverse of vertical-plane orbit feed path-length response matrix for beamline RING of lattice optics

Correctors

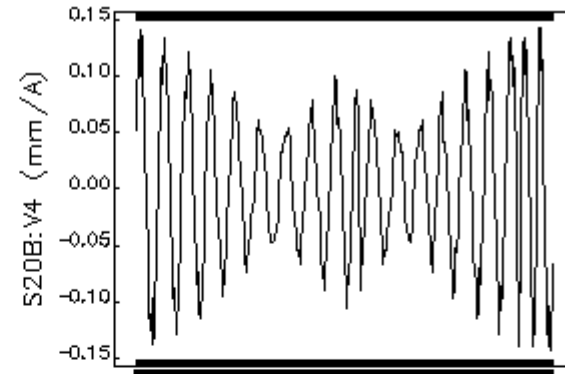


A Better Bump - 4 by 394 Response Matrix

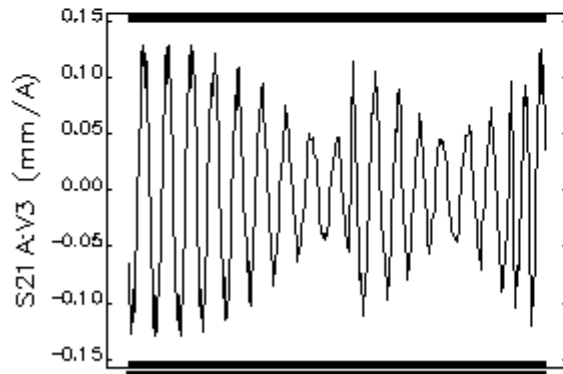
Correctors



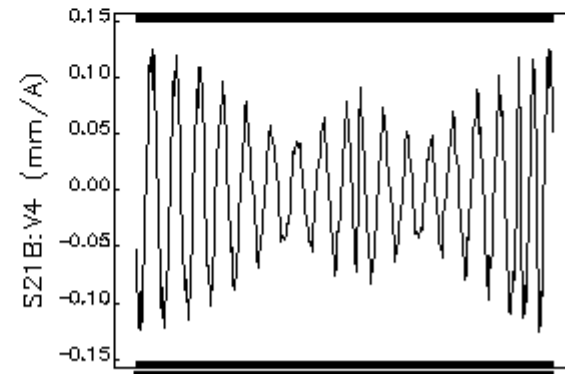
verified-phase orbit feed path-length response matrix for baseline RDM of lattice sys.for



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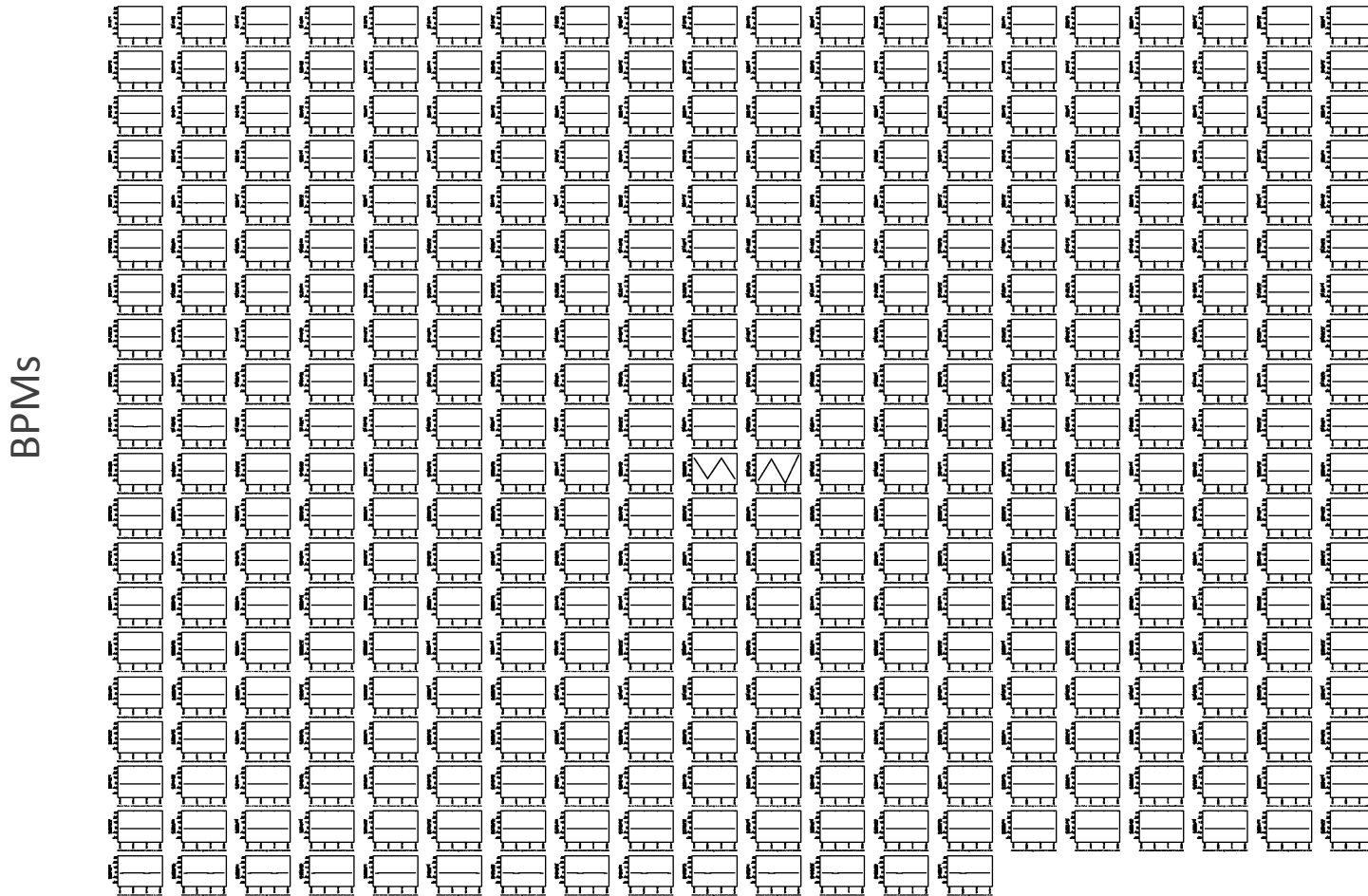
BPMs

Vertical Tune is 19.3



4 by 394 Pseudo-Inverse Response Matrix

$$Y_m = R_{mn} C_n \quad R = U S V^T \quad C_n = R_{nm}^{-1} Y_m$$

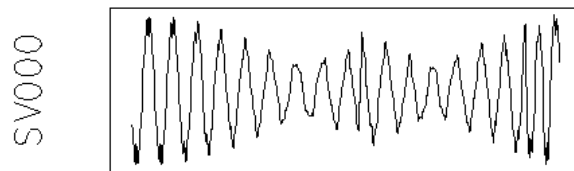


4 by 394 U Matrix - Eigenorbits

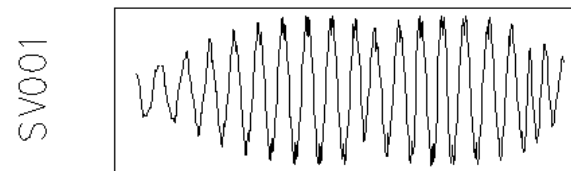
$$Y_m = R_{mn} C_n$$

$$R = U S V^T$$

$$C_n = R_{nm}^{-1} Y_m$$

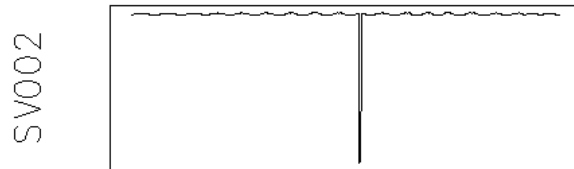


OriginalRows
U column-orthogonal matrix



OriginalRows
U column-orthogonal matrix

Bump leakage

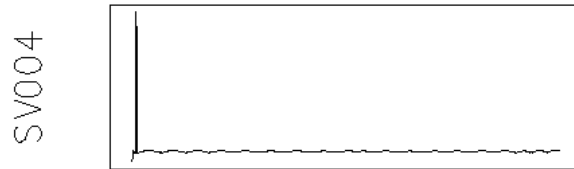


OriginalRows
U column-orthogonal matrix

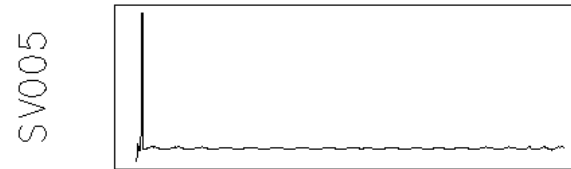


OriginalRows
U column-orthogonal matrix

Parallel translation
And angle bumps

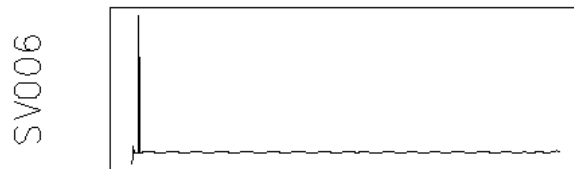


OriginalRows
U column-orthogonal matrix

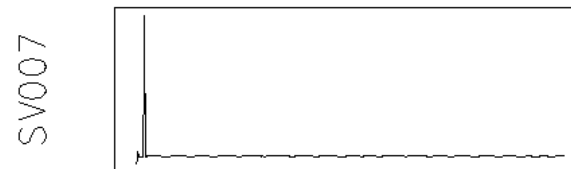


OriginalRows
U column-orthogonal matrix

Single-BPM
impulses



OriginalRows
U column-orthogonal matrix



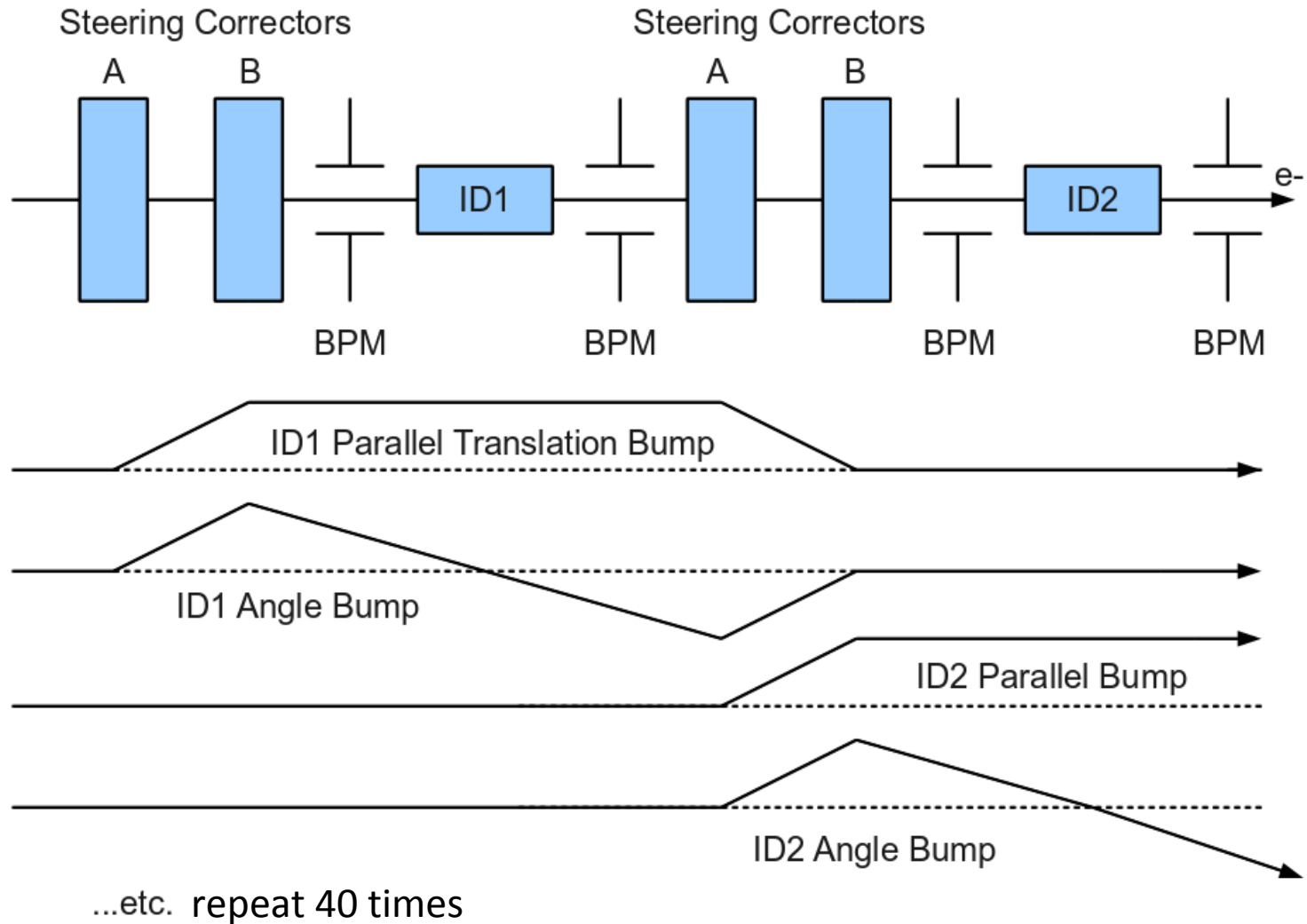
OriginalRows
U column-orthogonal matrix

A case where lots of BPMS are a good thing

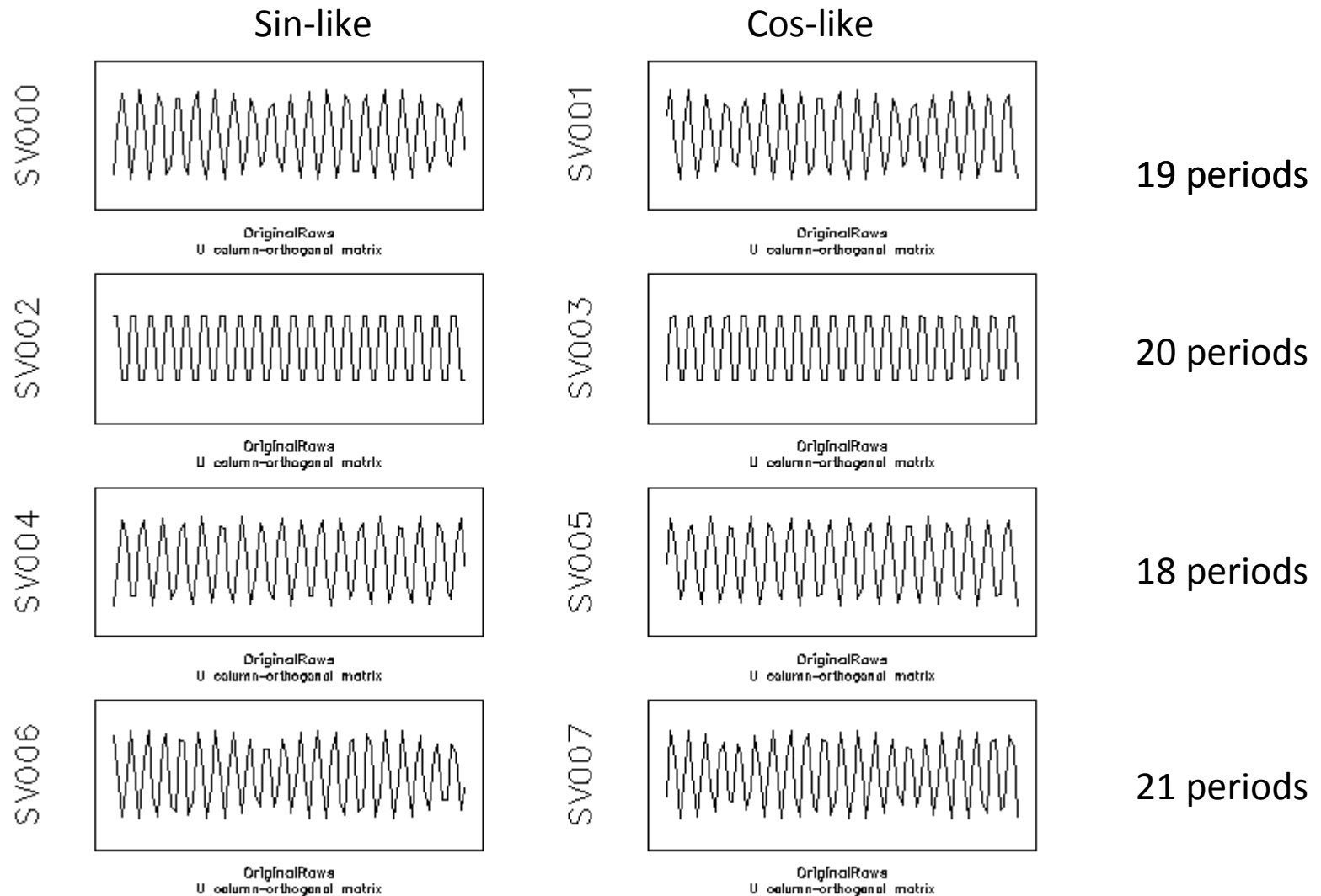


Spatial Modes 2 - An Eighty by Eighty Square Matrix

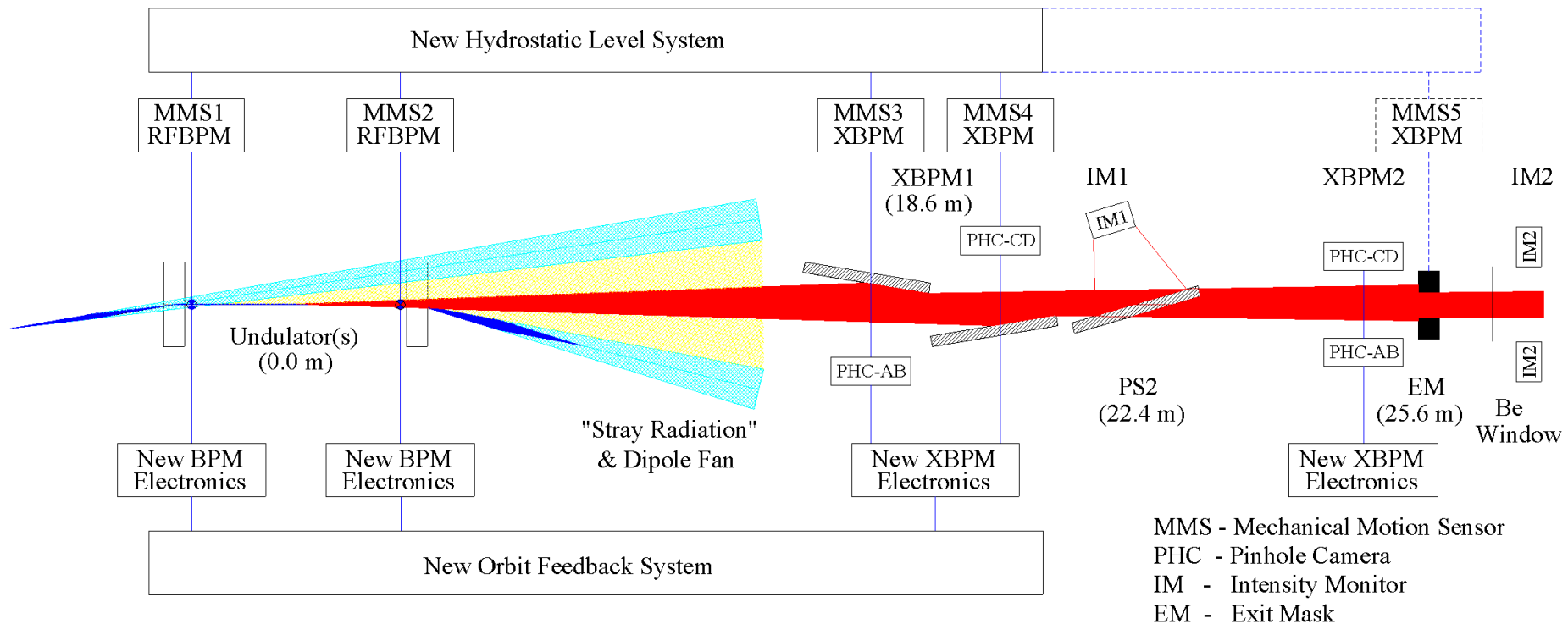
glennsSquareMatrix Example



glennsSquareMatrix U Matrix Eigenorbits



Thinking Locally - Sector 27 in September 2014

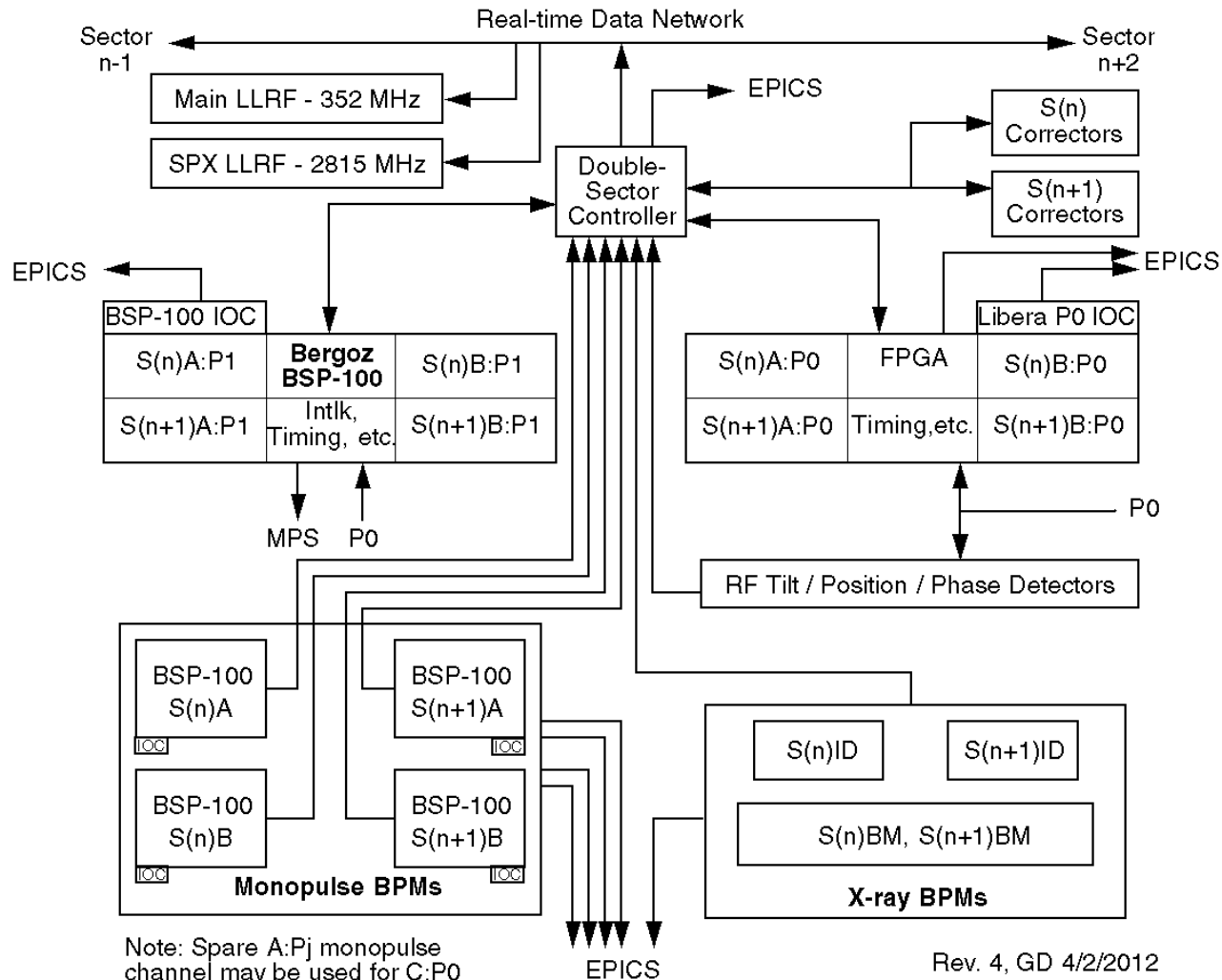


- Consider doing exact full-band correction on only source RF bpps using something like glennsSquareMatrix.
- Then use second much slower feedback connecting xbps to rfbpm setpoints.
- Worry about BM beamlines later, perhaps with calibrated slow corrector bumps
- End of digression

What will it look like

Proposed Real-Time Feedback Double-Sector* Architecture (Revision 4)

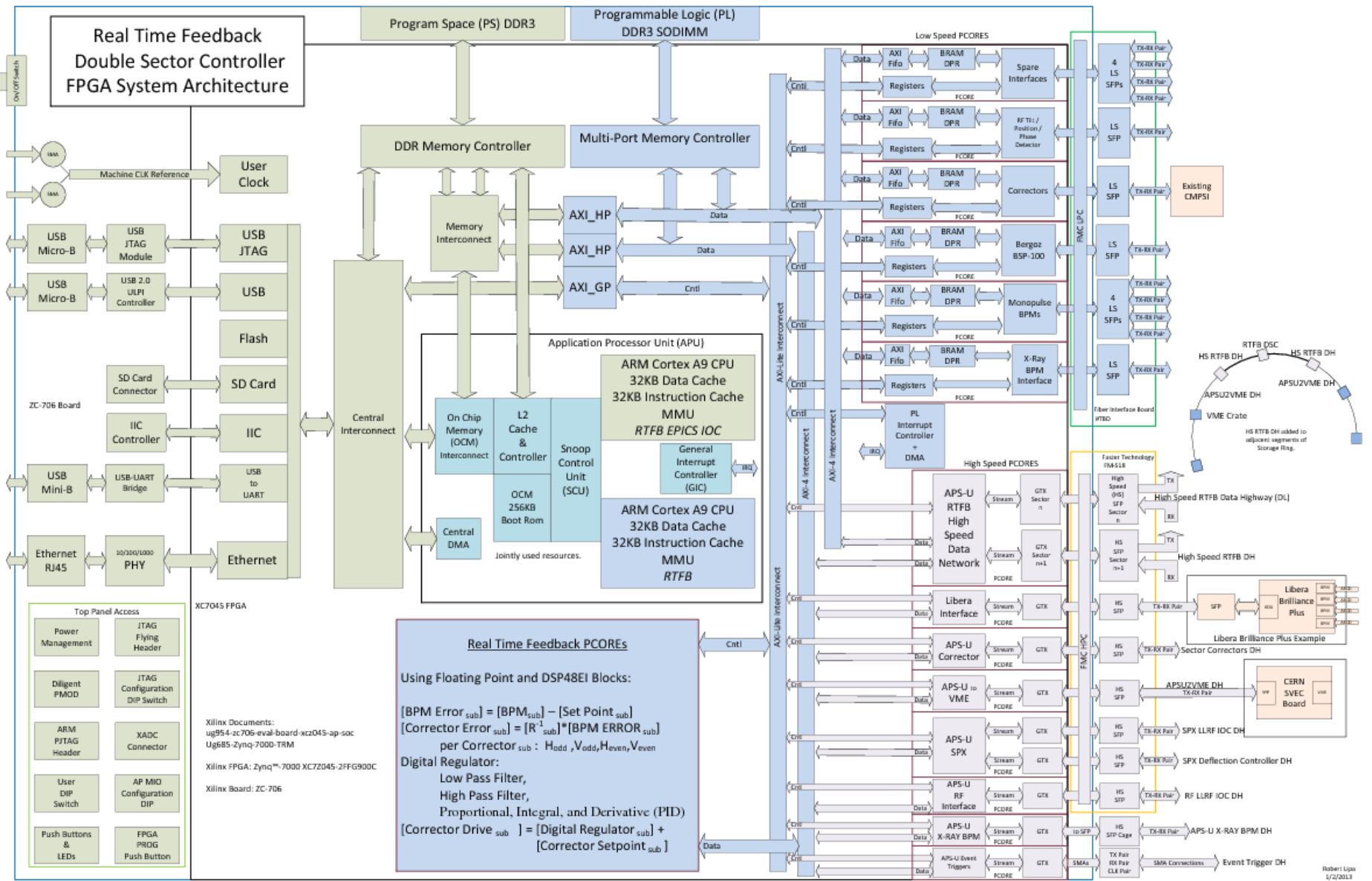
* Note n is odd



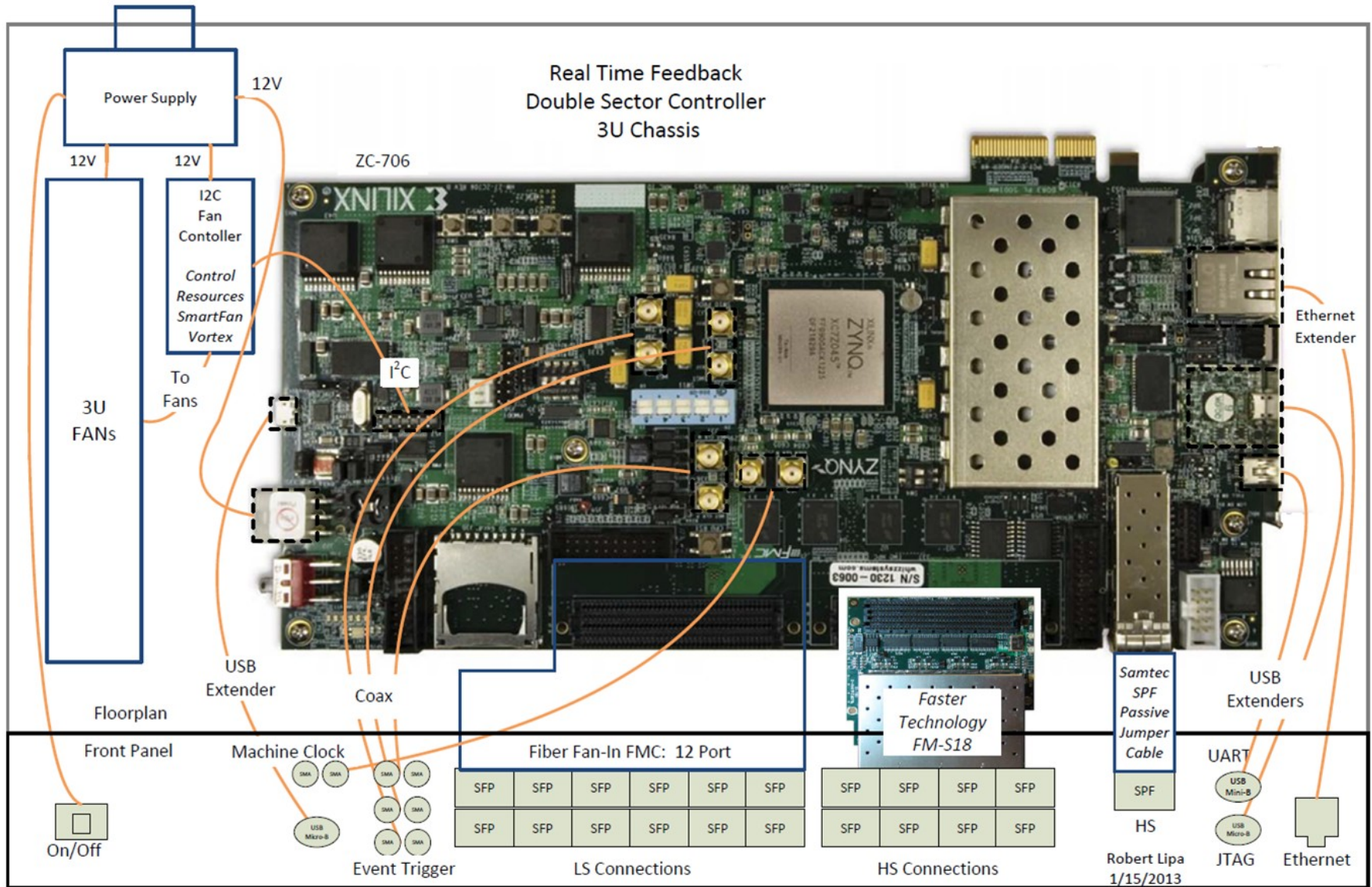
22.6 vs. 1.5 kHz
Access to everything
Nominal 200 Hz
Closed-loop BW

Rev. 4, GD 4/2/2012

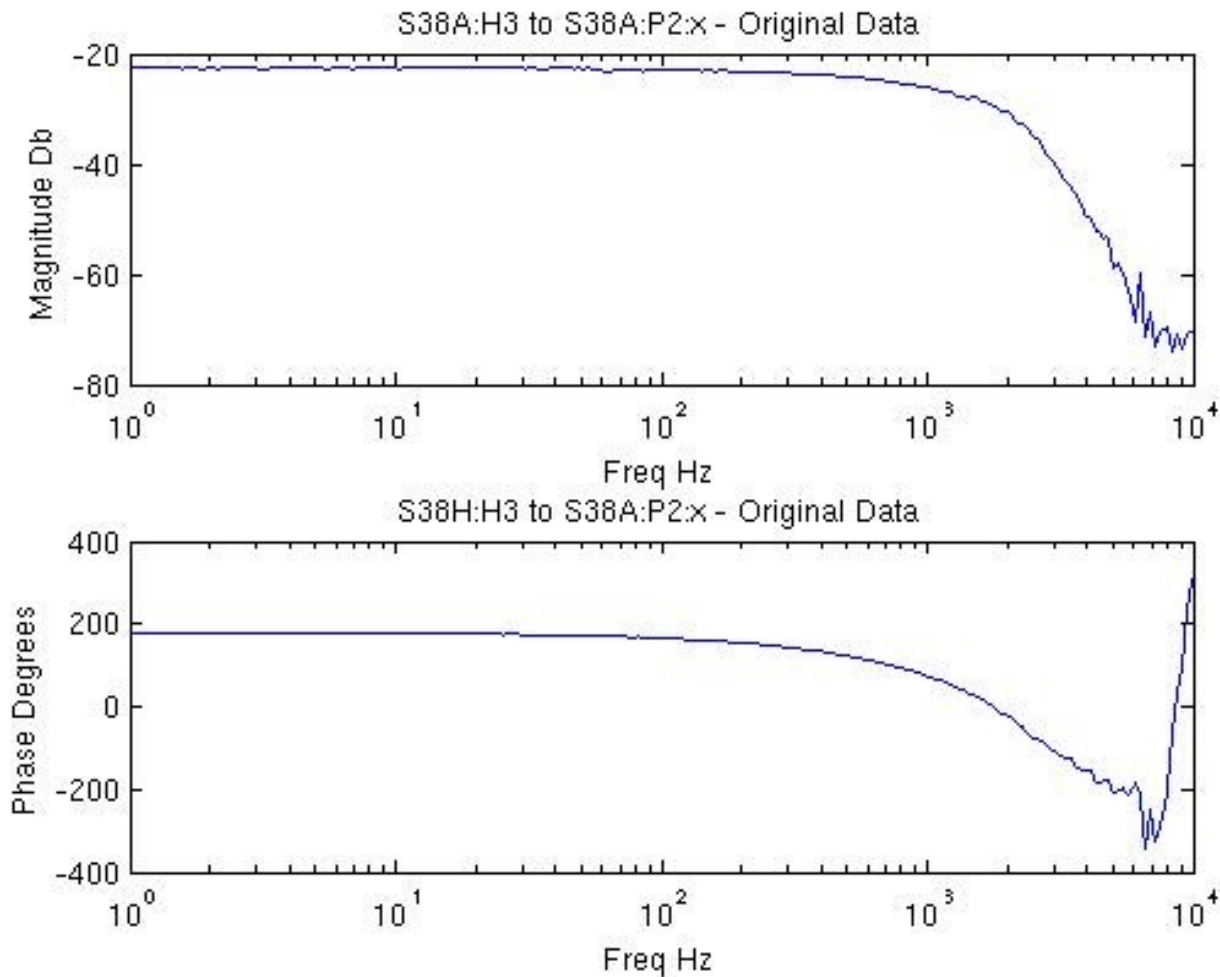
Double Sector Controller Architecture



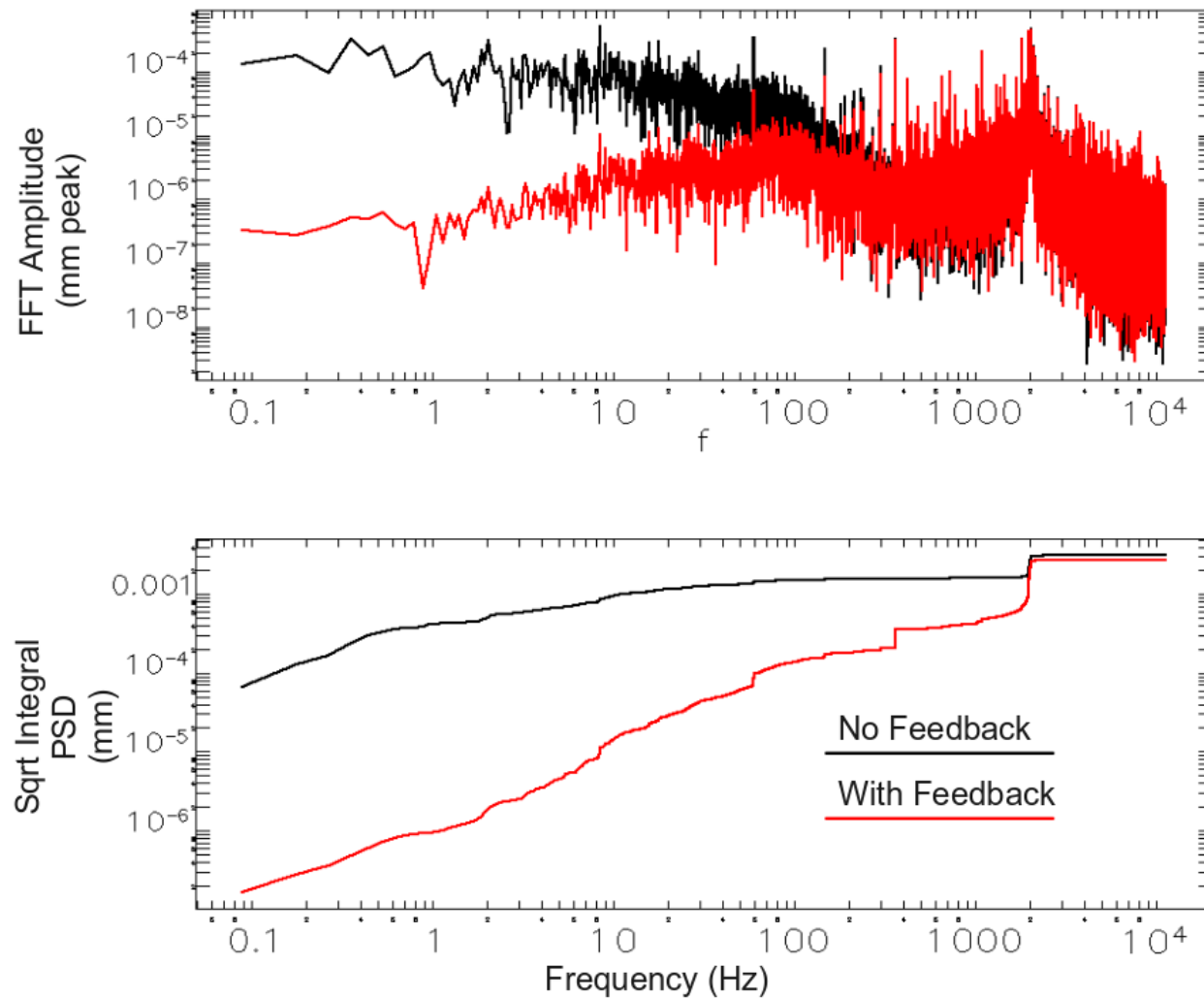
Zynq Board Interfaces



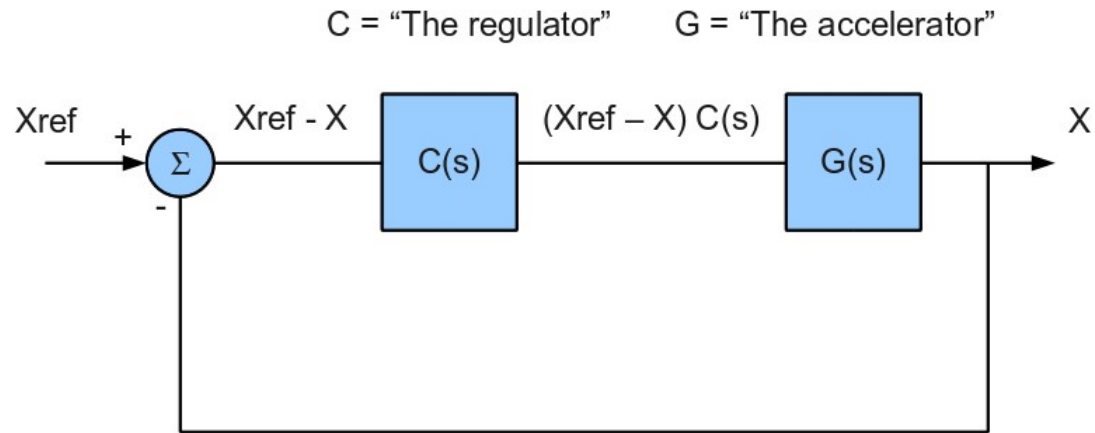
Measured Response S38A:H3 to S38A:P2x Raw



Simulation



Implementation



$$(X_{\text{ref}} - X) C(s) G(s) = X$$

$$\frac{X}{X_{\text{ref}}} = \frac{C G}{1 + C G}$$

Summary

- APS feedback design is constrained by
 - Existing hardware,
 - 5000 hour operating schedule throughout
 - Installation during three month-long shutdowns / year, 10 total
- Design process is
 - To learn from our own and other's mistakes (this workshop)
 - Comprehensive measurements on the existing accelerator
 - Simulation to refine algorithms in space and time
- First dress rehearsal summer 2014
- Operational deployment September 2014

